

# REAL OPTION VALUE

## CHAPTER 7 SEQUENTIAL INVESTMENT OPTIONS

Thus far, it has been assumed that the investment is completed instantaneously upon exercise of the real option, that is when commencing the investment. Often, investment opportunities require a sequence of expenditures, so that interim “mini-investments” are necessary over a time line in order to keep the ultimate investment opportunity option alive. This chapter allows for sequential investment options (also termed instalment options), where it is assumed that interim expenditures are completely sunk costs, having no alternative or scrap value.

Assume first the investment program involves required initial expenditures (the real option premium), a second phase of required investment expenditures ( $D$ ), and a final development phase, when then the project values ( $V$ ) are realized. The essential aspect of this characterized program is that managers have a choice of whether to pay the interim expenditure, and then the development cost ( $K$ ). This program constitutes a call option on a further call option. If all costs are considered “sunk costs”, the initial expense at  $t_0$  is an irrecoverable premium for a call option to pay  $D$  at  $t_1$ , which is itself a premium for an option to pay  $K$  at  $t_2$ , to receive then the project values. Without management flexibility not to pay  $D$  or  $K$ , perhaps such a program should be valued using present values. With management discretion, real option models are appropriate since future expenditures can be cancelled. The first stage decisions are based on the difference between perceived value (including future options) and investment cost at or before exercise dates. The transitions between the stages are sequential options.

These models are suitable for any investment program, where there are required interim expenditures for program continuance such as: (a) a telecommunications company contemplating providing intermediate services and looking to maintain or

increase line usage, or a mobile operator initially bidding for a 4G license, that requires R&D at a first stage, and then implementation expenditures; (b) an E\_Commerce software or a search service provider, which aims to add advertising, and then content in sequences, each requiring R&D and marketing expenditures; (c) a property developer, who pays an initial price for development land, where there are required interim decontamination expenses, and then final construction costs; and (d) a R&D venture where both the investment cost and probability of success increase over the stages.

Here are three real option valuation methods, starting with a simple European compound option, extended to a European compound exchange option. Finally, an American perpetual exchange option is presented, allowing for several stages of investment expenditures (and critical threshold values which justify making those expenditures).

The simplest European sequential model is the Geske (1979) compound call on a call option. The simple European exchange option is an adapted Margrabe (1978) exchange option, set in a compound option format. This assumes that both the development costs and the ultimate project value are both stochastic, and costs (D) must be spent at  $t_1$  in order to keep alive the option to exchange K for V at  $T(=t_2)$ . Building on Adkins and Paxson (2013, 2016), a multi-stage sequential American perpetual exchange model is provided.

## 7.1 SEQUENTIAL EUROPEAN REAL OPTIONS

Geske (1979) developed an analytic framework for a European option, where in order to keep the option alive an interim expenditure is required. There is a critical value  $V^*$  which justifies making the interim expenditure. Assume that developed values (V) follow a geometric Brownian motion:

$$dV = (\mu_V - \delta_V)Vdt + \sigma_V Vdz_V \quad (7.1)$$

where  $\mu_V$  is the equilibrium expected drift rate,  $\delta_V$  is the income rate (or payout rate) of  $V$ , and  $\sigma_V$  is the volatility. Let the value of a call on a call be the real option value  $C_c$ , where  $D$  is the interim expenditure required at time  $\tau'=.5$  (or another fraction), and  $K$  the investment cost at time  $\tau$ . The value of a call on a call  $C_c$  is given by

$$C_c = Ve^{-\delta\tau} B(a_1, d_1; \rho) - Ke^{-r(\tau-\tau')} B(a_2, d_2; \rho) - De^{-r\tau'} N(a_2) \quad (7.2)$$

where  $\rho$  is the correlation coefficient between the overlapping Brownian motion increments, which is defined as  $\rho = \sqrt{\tau'/\tau}$ , and  $N(\cdot)$  and  $B(\cdot)$  are the standard cumulative univariate and bivariate normal distributions with parameters:

$$a_1 = \frac{\ln(V/V^*) + (r - \delta + 0.5\sigma^2)\tau'}{\sigma\sqrt{\tau'}}, \quad a_2 = a_1 - \sigma\sqrt{\tau'}, \quad (7.3)$$

$$d_1 = \frac{\ln(V/K) + (r - \delta + 0.5\sigma^2)\tau}{\sigma\sqrt{\tau}}, \quad d_2 = d_1 - \sigma\sqrt{\tau}.$$

The critical price,  $V^*$ , is obtained by solving the value matching condition:

$$V^* e^{-\delta(\tau-\tau')} N(d_1^*) - Ke^{-r(\tau-\tau')} N(d_2^*) = D \quad (7.4)$$

$$d_1^* = \frac{\ln(V^*/K) + (r - \delta + 0.5\sigma^2)(\tau - \tau')}{\sigma\sqrt{\tau - \tau'}}, \quad d_2^* = d_1^* - \sigma\sqrt{\tau - \tau'} \quad (7.5)$$

Using base case parameter values, the Geske European sequential investment model is shown in Figure 7.1. Use Data/Solver to solve equation (7.4)- $D=0$ . In column B,  $V^*$  is 95, almost the current value of 100, for this is a more or less an at-the-money compound call option. If  $V$  is 100 at time  $\tau'$ , the payment  $D=20$  should be made in order to keep the ultimate call option alive.

Since the Geske compound option model is European, it is at best a first estimate for long-lived sequential options. As also shown in Figure 7.1 column C, the compound option value increases as the time to ultimate exercise increases (with  $D$  at the half way time).

Figure 7.1

	A	B	C	D
1	<b>GESKE EUROPEAN COMPOUND CALL OPTION</b>			
2				
3	DEVELOPMENT TIME $\tau'$	1	3.00	
4	INVESTMENT TIME $\tau$	2	3.75	
5	INTEREST RATE	0.04	0.04	
6	V YIELD	0.04	0.04	
7	VALUE VOLATILITY	0.20	0.20	
8	V	100.00	100.00	
9	D	10.00	10.00	
10	K	90.00	90.00	
11	<b>REAL OPTION VALUE</b>	<b>7.9079</b>	<b>11.9899</b>	$B8*EXP(-B6*B4)*B26-B10*EXP(-B5*B4)*B27-B9*EXP(-B5*B3)*B25$
12	$\tau-\tau'$	1.00	0.75	$B4-B3$
13	$V^*$	95.42	96.65	
14	$d_1$	0.39	0.50	$(LN(B13/B10)+((B5-B6+0.5*B7^2)*B12))/(B7*SQRT(B12))$
15	$d_2$	0.19	0.33	$B14-B7*SQRT(B12)$
16	$N_1$	0.65	0.69	$NORMSDIST(B14)$
17	$N_2$	0.58	0.63	$NORMSDIST(B15)$
18	EQ 7.4	10.00	10.00	$B13*EXP(-B6*B12)*B16-B10*EXP(-B5*B12)*B17$
19	EQ 7.4-D	0.00	0.00	$B18-B9$
20	$\rho(\tau'/\tau)$	0.71	0.89	$SQRT(B3/B4)$
21	$d_{1,t1}$	0.33	0.27	$(LN(B8/B13)+((B5-B6+0.5*B7^2)*B3))/(B7*SQRT(B3))$
22	$d_{1,t2}$	0.51	0.47	$(LN(B8/B10)+((B5-B6+0.5*B7^2)*B4))/(B7*SQRT(B4))$
23	$d_{2,t1}$	0.13	-0.07	$B21-B7*SQRT(B3)$
24	$d_{2,t2}$	0.23	0.08	$B22-B7*SQRT(B4)$
25	$N_2$	0.55	0.47	$NORMSDIST(B23)$
26	$B_1$	0.55	0.57	$BiVariateNormalCDF(B21,B22,B20)$
27	$B_2$	0.45	0.42	$BiVariateNormalCDF(B23,B24,B20)$
28				
29	The first five inputs are the D and K timing estimates, the interest rate, and the			
30	value yield and volatility.			
31	The next three inputs are V, D and K estimates.			
32	Real call option value assumes $V^*$ is the value above which D should be paid at $\tau'$ .			
33	USE TOOLS/SOLVER, SETTING B19=0 BY CHANGING B13.			

## 7.2 SEQUENTIAL EUROPEAN EXCHANGE OPTION

It is easy to extend this compound option model to a European sequential exchange real option. Suppose that the D and development costs K follow a diffusion process similar to that for V:

$$dK = (\mu_K - \delta_K)Kdt + \sigma_K Kdz_K \quad (7.6)$$

where  $\mu_K$  is the drift term (the expected cost escalation),  $\delta_K$  is the payout rate on similar investment cost businesses,  $\sigma_K$  is the volatility of the investment cost, and

the correlation between the Wiener processes is  $\rho$ . Assuming that the exercise price of the first (compound) option,  $D$ , is expressed as a fixed proportion (Q%) of  $K$ , i.e.,  $D=QK$ , Carr (1988) gives the solution for the European compound exchange call option:

$$w_C(V, K, D, \tau, \tau') = Ve^{-\delta_V \tau} B\left(a_1, b_1; \sqrt{\frac{\tau'}{\tau}}\right) - Ke^{-\delta_K \tau} B\left(a_2, b_2; \sqrt{\frac{\tau'}{\tau}}\right) - De^{-\delta_K \tau'} N(a_2) \quad (7.7)$$

where

$$a_1 = \frac{\ln(X / X^*) + (\delta_K - \delta_V + 0.5\sigma^2)\tau'}{\sigma\sqrt{\tau'}}, \quad a_2 = a_1 - \sigma\sqrt{\tau'}, \quad (7.8)$$

$$b_1 = \frac{\ln(X) + (\delta_K - \delta_V + 0.5\sigma^2)\tau}{\sigma\sqrt{\tau}}, \quad b_2 = b_1 - \sigma\sqrt{\tau}, \quad (7.9)$$

$$X = \frac{V}{K}, \quad \sigma = \sqrt{\sigma_V^2 - 2\rho\sigma_V\sigma_K + \sigma_K^2}.$$

$N(\cdot)$  and  $B(\cdot, \cdot; \cdot)$  are the standard normal cumulative univariate and bivariate distributions. At time  $\tau'$ , one would exercise the compound call and obtain the underlying European exchange call option if the critical price-cost ratio is such that  $X^* < X_{\tau'}$ . The critical ratio,  $X^*$ , above which the compound option should be exercised at time  $\tau'$  can be obtained using the solution for the European exchange call option:

$$X^* e^{(\delta_K - \delta_V)(\tau - \tau')} N(b_1^*) - N(b_2^*) = Q \quad (7.10)$$

where

$$b_1^* = \frac{\ln(X^*) + (\delta_K - \delta_V + 0.5\sigma^2)(\tau - \tau')}{\sigma\sqrt{\tau - \tau'}}, \quad b_2^* = b_1^* - \sigma\sqrt{\tau - \tau'} \quad (7.11)$$

Figure 7.2

	A	B	C
1	<b>EUROPEAN COMPOUND EXCHANGE OPTION</b>		
2			
3	DEVELOPMENT TIME $\tau'$	1	
4	INVESTMENT TIME $\tau$	2	
5	V YIELD	0.04	
6	K YIELD	0.04	
7	VALUE VOLATILITY	0.20	
8	K VOLATILITY	0.20	
9	CORRELATION	0.50	
10	EXCHANGE VOLATILITY	0.20	SQRT(B7^2+B8^2-2*B9*B7*B8)
11	V	100.00	
12	D	10.00	
13	K	90.00	
14	X=V/K	1.1111	B11/B13
15	<b>REAL OPTION VALUE</b>	<b>7.9075</b>	B11*EXP(-B5*B4)*B30-B13*EXP(-B6*B4)*B31-B12*EXP(-B6*B3)*B29
16	$\tau-\tau'$	1.00	B4-B3
17	X*	1.06	
18	d1	0.63	(LN(B11/B13)+((B5-B6+0.5*B10^2)*B16))/(B10*SQRT(B16))
19	d2	0.43	B18-B10*SQRT(B16)
20	N1	0.73	NORMSDIST(B18)
21	N2	0.67	NORMSDIST(B19)
22	EQ 7.10	0.11	B17*EXP(-B5*B16)*B20-EXP(-B6*B16)*B21
23	EQ 7.10-D/K	0.00	B22-(B12/B13)
24	$\rho(\tau'/\tau)$	0.71	SQRT(B3/B4)
25	d1,t1	0.32	(LN(B14/B17)+(B6-B5+0.5*B10^2)*B3)/(B10*SQRT(B3))
26	d1,t2	0.51	(LN(B14)+(B6-B5+0.5*B10^2)*B4)/(B10*SQRT(B4))
27	d2,t1	0.12	B25-B7*SQRT(B3)
28	d2,t2	0.23	B26-B7*SQRT(B4)
29	N2	0.55	NORMSDIST(B27)
30	B1	0.54	BiVariateNormalCDF(B25,B26,B24)
31	B2	0.45	BiVariateNormalCDF(B27,B28,B24)
32			
33	The first five inputs are the D and K timing estimates, the		
34	value and cost yields and volatilities, and correlation.		
35	After calculating the exchange volatility, the next three inputs are V, D and K estimates.		
36	Real call option value assumes X* is the value above which D should be paid at $\tau'$ .		
37	USE TOOLS/SOLVER, SETTING B23=0 BY CHANGING B17.		

The European sequential option model assumes that D cannot occur until  $\tau'$  and K is only paid or exercised at  $\tau$ . This is mechanical, and does not allow management any flexibility, except to choose whether to make the investment decisions. The input parameters are chosen so that the ROV is the same as in the previous figure. Different inputs for K yield and volatility, and correlation, will yield different results.

### **7.3 AMERICAN SEQUENTIAL MULTI-STAGE EXCHANGE REAL OPTIONS**

This section provides a model for evaluating a multiple stage sequential investment opportunity without resort to a multivariate distribution function. The analytical solution depends on assuming a probability of catastrophic failure at each investment stage that declines as the project nears completion, which is a characteristic of many R&D, exploration and infrastructure projects. The project can then be interpreted as a collection of investment stages, such that no stage investment, except the first, can be started until the preceding stage has been completed. Success at each stage is not guaranteed because of the possibility of a catastrophic failure that reduces the option value to zero. The project value is realized when all the stages have been successfully completed. A typical four-stage opportunity involves: (i) undertaking basic research. (ii) developing a marketable product, (iii) testing its viability and (iv) implementing the infrastructure for launch and delivery. Multiple sequential investment opportunities are common amongst industries as diverse as oil exploration and mining, aircraft manufacture, pharmaceuticals and consumer electronics.

Schwartz and Moon (2000) model a new drug development process which consists of four distinct phases, each with a positive probability of failure, although not necessarily declining over time. Cortazar, Schwartz and Casassus (2003) describe four natural resource exploration stages of a project with technical success probability increasing over each phase, and then a production phase which is subject to commodity price uncertainty. Pennings and Sereno (2011) study the development path of a new medicine over seven phases, with a probability of failure declining over time.

Making an investment at a stage depends on whether the prevailing project value is of sufficient magnitude to economically justify committing the investment cost, or whether it is more desirable to wait for more favorable conditions. There are three

sources of uncertainty, the stochastic project value and the investment cost, and the probability of a catastrophic failure, which are considered in a closed-form rule for the investment decision at each of the project stages.

Other authors simplify the multiple investment stage problems for obtaining a meaningful solution. Building on the valuation of sequential exchange opportunities by Carr (1988), Lee and Paxson (2001) use an element of European style compound options (and approximation of an American option phase) for formulating a two-stage sequential investment. Brach and Paxson (2001) examine a two-stage sequential investment opportunity similar to the formulation currently under study but they confine their attention more to valuation. Childs and Triantis (1999) formulate a multiple sequential investment model with interaction and obtain a solution through using a trinomial lattice. For all of these expositions, the solution is either not analytical or is restricted to only two stages.

Cassimon et al. (2004) study American-type investment options, but provide a solution based on the complex multivariate distribution available in some mathematical programmes. Building on Adkins and Paxson (2011), Adkins and Paxson (2013) suggest an analytic solution for N-stage sequential investments.

Consider an investment project made up of a discrete number of sequential stages, each involving an individual non-zero investment cost. The project as an entity is not fully implemented and the project value not realized until all of the sequential stages have been successfully completed. Each successive investment stage relies on the successful completion of the investment made at the preceding stage, but the stage timing is not specified. Each investment stage is ordered by the number  $J$  of remaining stages, including the current one, until project completion. The decision making position is first examined for the ultimate stage where  $J = 1$ , and then by replication for the preceding stages, incrementally. At the ultimate stage, the decision whether or not to make an investment in a real asset is decided by whether



or not the option value at  $J = 1$  fully compensates the expected net present value of the cash flow stream rendered by the asset. At the penultimate stage  $J = 2$ , whether to make an expenditure to obtain the investment option at  $J = 1$  depends on whether or not the option value at  $J = 2$  fully compensates for the net option value at  $J = 1$ . This procedure is then replicated incrementally for stages greater than 2.

A representation of the sequential investments process for a  $J = N$  stage project is illustrated in Figure 7.3. This figure shows an ordered sequence of stage investments, where after an investment, the possible outcomes are success and failure. If all the stage outcomes are successful, then the entire project is successfully completed and its value can be realized. Although the investment is committed, the stage may not be successfully completed owing to fundamental irresolvable technical or market impediments, in which case, the option value instantly falls to zero and the project is abandoned without any value. The probability of failure at stage  $J$  is denoted by  $\lambda_j$  where  $0 \leq \lambda_j < 1 \forall J$ .

Situations where an investment can produce an innovative breakthrough and generate an unanticipated increase in the project value are ignored. Also, other forms of optionality, such as terminating a project before completion for its abandonment value, are not considered.

The value of the project is defined by  $V$ . The investment expenditure made at any stage  $J$  is denoted by  $K_j$  for all possible values of  $J$ . Both the project value and the set of investment expenditures are treated as stochastic. It is assumed that they are individually well described by the geometric Brownian motion process:

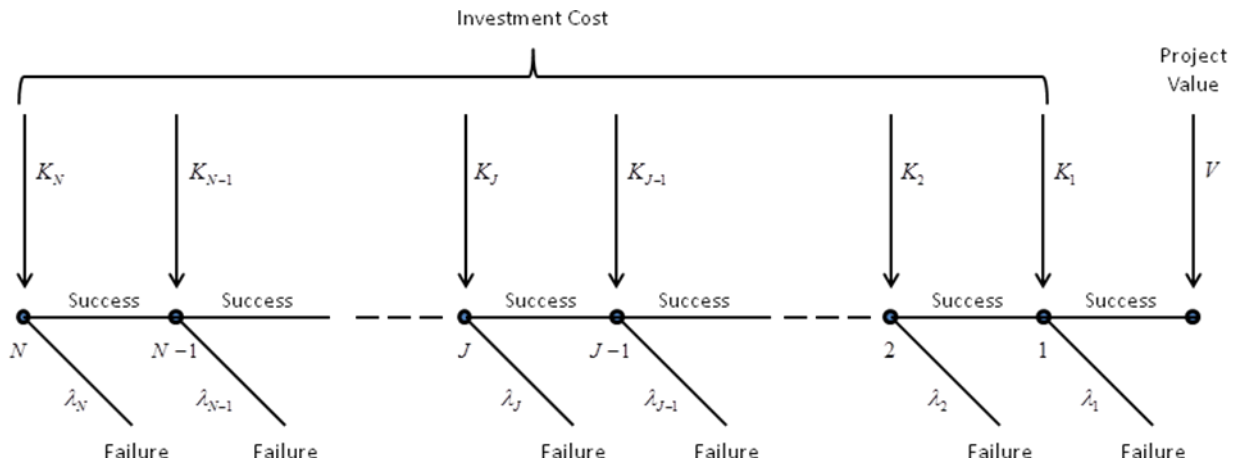
$$dX = \alpha_x X dt + \sigma_x X dz_x \quad (7.12)$$

for  $X \in \{V, K_j \forall J\}$ , where  $\alpha_x$  represent the respective drift parameters,  $\sigma_x$  the respective instantaneous volatility parameter, and  $dz_x$  the respective increment of a standard Wiener process. Dependence between any two of the factors is represented

by the covariance term; so, for example, the covariance between the real asset value and the investment expenditure at stage  $J$  is specified by:

$$\text{Cov}[dV, dK_J] = \rho_{VK_J} \sigma_V \sigma_{K_J} dt.$$

Figure 7.3  
**Sequential Investment Process**



Different stages may have different factor volatilities and correlations. The risk-free rate is  $r$ , and the investment expenditure at each stage  $K$  is assumed to be instantaneous.

### One-Stage Model

The final stage  $J = 1$  model represents the investment opportunity for developing a project value  $V$  following the investment cost  $K_1$ , given that the research effort may fail totally with probability  $\lambda_1$ . The value  $F_1$  of the investment opportunity at stage  $J = 1$  depends on the project value and the investment cost, so  $F_1 = F_1(V, K_1)$ . By Ito's lemma, the risk neutral valuation relationship is:

$$\begin{aligned} \frac{1}{2}\sigma_V^2 V^2 \frac{\partial^2 F_1}{\partial V^2} + \frac{1}{2}\sigma_{K_1}^2 K_1^2 \frac{\partial^2 F_1}{\partial K_1^2} + \rho_{VK_1} \sigma_V \sigma_{K_1} VK_1 \frac{\partial^2 F_1}{\partial V \partial K_1} \\ + \theta_V V \frac{\partial F_1}{\partial V} + \theta_{K_1} K_1 \frac{\partial F_1}{\partial K_1} - (r + \lambda_1) F_1 = 0, \end{aligned} \quad (7.13)$$

where the  $\theta_X$  for  $X \in \{V, K_J \forall J\}$  denote the respective risk neutral drift rate parameters. The generic solution is the two-factor power function:

$$F_1 = A_1 V^{\beta_1} K_1^{\eta_1}, \quad (7.14)$$

where  $\beta_1$  and  $\eta_1$  denote the generic unknown parameters for the two factors, project value and investment cost, and  $A_1$  denotes a generic unknown coefficient. Since the option value is always non-negative,  $A_1 \geq 0$ . We conjecture that  $\beta_1 \geq 0$  and  $\eta_1 < 0$ , and  $\beta_1 + \eta_1 = 1$ . The power parameter values satisfy the characteristic root function:

$$Q_1(\beta_1, 1 - \beta_1) = \frac{1}{2}\sigma_1^2 \beta_1 (\beta_1 - 1) + \beta_1 (\theta_V - \theta_{K_1}) - (r + \lambda_1 - \theta_{K_1}) = 0, \quad (7.15)$$

$$\text{where } \sigma_1^2 = \sigma_V^2 + \sigma_{K_1}^2 - 2\rho_{V,K_1} \sigma_V \sigma_{K_1}. \quad (7.16)$$

The threshold levels for the project value and the investment cost signaling the optimal exercise for the investment option at stage  $J = 1$  are denoted by  $\hat{V}_1$  and  $\hat{K}_1$ , respectively. The value matching relationship describes the conservation equality at optimality that the option value  $\hat{F}_1 = F_1(\hat{V}_1, \hat{K}_1)$  exactly compensates the net asset value  $\hat{V}_1 - \hat{K}_1$ . Then:

$$A_1 \hat{V}_1^{\beta_1} \hat{K}_1^{\eta_1} = \hat{V}_1 - \hat{K}_1. \quad (7.17)$$

There are two associated smooth pasting conditions, one for each factor, which can be expressed as:

$$A_1 \hat{V}_1^{\beta_1} \hat{K}_1^{\eta_1} = \frac{\hat{V}_1}{\beta_1}. \quad (7.18)$$

$$A_1 \hat{V}_1^{\beta_1} \hat{K}_1^{\eta_1} = -\frac{\hat{K}_1}{\eta_1} \quad (7.19)$$

Further, the threshold levels are related by:

$$\hat{V}_1 = \frac{\beta_1}{\beta_1 - 1} \hat{K}_1, \quad (7.20)$$

with 
$$A_1 = \beta_1^{-\beta_1} (\beta_1 - 1)^{\beta_1 - 1}. \quad (7.21)$$

### Two-Stage Model

At the preceding stage,  $J = 2$ , the viability of committing an investment  $K_2$  to acquire the option to invest  $F_1$  is compared to the value of the compound option  $F_2$  with the net benefits  $F_1 - K_2$ .  $F_2$  depends on the three factors  $V$ ,  $K_1$  and  $K_2$ , so  $F_2 = F_2(V, K_1, K_2)$ . By Ito's lemma, the risk neutral valuation relationship for  $F_2$  is:

$$\begin{aligned} & \frac{1}{2} \sigma_V^2 V^2 \frac{\partial^2 F_2}{\partial V^2} + \frac{1}{2} \sigma_{K_1}^2 K_1^2 \frac{\partial^2 F_2}{\partial K_1^2} + \frac{1}{2} \sigma_{K_2}^2 K_2^2 \frac{\partial^2 F_2}{\partial K_2^2} \\ & + \rho_{V, K_1} \sigma_V \sigma_{K_1} V K_1 \frac{\partial^2 F_2}{\partial V \partial K_1} + \rho_{V, K_2} \sigma_V \sigma_{K_2} V K_2 \frac{\partial^2 F_2}{\partial V \partial K_2} + \rho_{K_1, K_2} \sigma_{K_1} \sigma_{K_2} K_1 K_2 \frac{\partial^2 F_2}{\partial K_1 \partial K_2} \quad (7.22) \\ & + \theta_V V \frac{\partial F_2}{\partial V} + \theta_{K_2} K_2 \frac{\partial F_2}{\partial K_2} + \theta_{K_1} K_1 \frac{\partial F_2}{\partial K_1} - (r + \lambda_2) F_2 = 0. \end{aligned}$$

The solution to (7.22) is a product power function, with generic form:

$$F_2 = A_2 V^{\beta_2} K_1^{\eta_{21}} K_2^{\eta_{22}} = B_2 [F_1]^{\phi_2} K_2^{1 - \phi_2} \quad (7.23)$$

where  $\beta_2$ ,  $\eta_{21}$  and  $\eta_{22}$  denote the generic unknown parameters for the three factors, project value and investment expenditure at stage-one and -two respectively, the first subscript denotes the stage, the second subscript the stage specific power parameter, and  $A_2$  denotes an unknown coefficient.  $B_2 = (\phi_2 - 1)^{(\phi_2 - 1)} / \phi_2^{\phi_2}$  (7.24)

The stage-two threshold levels signalling an optimal exercise are represented by  $\hat{V}_2$ ,  $\hat{K}_1$  and  $\hat{K}_2$  for  $V$ ,  $K_1$  and  $K_2$ , respectively. The set  $\{\hat{V}_2, \hat{K}_1, \hat{K}_2\}$  forms the boundary that discriminates between the ‘‘exercise’’ decision and the ‘‘wait’’ decision. The equilibrium amongst the threshold levels is the value matching relation that is expressed as:

$$A_2 \hat{V}_2^{\beta_2} \hat{K}_1^{\eta_{21}} \hat{K}_2^{\eta_{22}} = A_1 \hat{V}_2^{\beta_1} \hat{K}_1^{1-\beta_1} - \hat{K}_2, \quad (7.25)$$

where  $A_1$  and  $\beta_1$  are known from the evaluation for stage-one. There are three smooth pasting conditions, one for each of the three factors  $V$ ,  $K_1$  and  $K_2$ , respectively, can be expressed as:

$$\beta_2 A_2 \hat{V}_2^{\beta_2} \hat{K}_1^{\eta_{21}} \hat{K}_2^{\eta_{22}} = \beta_1 A_1 \hat{V}_2^{\beta_1} \hat{K}_1^{1-\beta_1}, \quad (7.26)$$

$$\eta_{21} A_2 \hat{V}_2^{\beta_2} \hat{K}_1^{\eta_{21}} \hat{K}_2^{\eta_{22}} = (1-\beta_1) A_1 \hat{V}_2^{\beta_1} \hat{K}_1^{1-\beta_1}, \quad (7.27)$$

$$\eta_{22} A_2 \hat{V}_2^{\beta_2} \hat{K}_1^{\eta_{21}} \hat{K}_2^{\eta_{22}} = -\hat{K}_2. \quad (7.28)$$

As a simplification in calculating the solution values, let  $\phi_2 = \beta_2 / \beta_1 \geq 0$ , then by using the substitutions  $\beta_2 = \phi_2 \beta_1$ ,  $\eta_{21} = (1-\beta_1) \phi_2$  and  $\eta_{22} = 1-\phi_2$ , the quadratic function  $Q_2$  can be expressed as:

$$Q_2 = \frac{1}{2} \phi_2 (\phi_2 - 1) \sigma_2^2 + \phi_2 (r + \lambda_1 - \theta_{K_2}) - (r + \lambda_2 - \theta_{K_2}) = 0. \quad (7.29)$$

where

$$\begin{aligned} \sigma_2^2 = & \beta_1^2 \sigma_V^2 + (1-\beta_1)^2 \sigma_{K_1}^2 + \sigma_{K_2}^2 \\ & + 2\beta_1(1-\beta_1) \rho_{VK_1} \sigma_V \sigma_{K_1} - 2\beta_1 \rho_{VK_2} \sigma_V \sigma_{K_2} - 2(1-\beta_1) \rho_{K_1 K_2} \sigma_{K_1} \sigma_{K_2}. \end{aligned} \quad (7.30)$$

The value of  $\phi_2$  is evaluated as the positive root of  $Q_2$ .

$$\hat{V}_2 = \frac{\beta_1}{\beta_1 - 1} \left\{ \frac{\phi_2 (\beta_1 - 1)}{\phi_2 - 1} \right\}^{\frac{1}{\beta_1}} \hat{K}_1^{\frac{\beta_1 - 1}{\beta_1}} \hat{K}_2^{\frac{1}{\beta_1}} \quad (7.31)$$

### Numerical Illustrations

Figure 7.4 is a spreadsheet evaluation on an illustration involving a 2-stage sequential investment project, solving two sets of simultaneous equations, EQs 7.15, 7.17, 7.18 and 7.19 for the first stage, and 7.25-7.29 for the second stage. The set of

probabilities of catastrophic failure at the stages adheres to the condition  $\lambda_1 < \lambda_2$ . Initially, the variances for the investment costs at the two stages have been set to be equal, the covariance terms between the four factors to equal zero, and the K thresholds are all assumed to be the same as the current value, so the threshold justifying investment at each stage is the ratio of  $\hat{V}$  to the nominal investment costs remaining.

Figure 7.4

	A	B	C	D	E	F	G	H	I	J	K
1	STAGE ONE		STAGE TWO								
2	INPUT										
3	V	100.00	100.00								
4	K1	90.00	90.00								
5	K2	10.00	10.00								
6	$\sigma V$	0.20	0.20								
7	$\sigma K1$	0.20	0.20								
8	$\sigma K2$	0.20	0.20								
9	$\rho VK1$	0.50	0.50								
10	$\rho VK2$	0.50	0.50								
11	$\rho K1K2$	0.00	0.00								
12	r	0.04	0.04								
13	$\theta V$	0.00	0.00								
14	$\theta K1$	0.04	0.04								
15	$\theta K2$	0.04	0.04								
16	$\lambda_1$	0.00	0.00								
17	$\lambda_2$	0.05	0.05								
18	OUTPUT										
19	$\sigma_1^2$	0.0400	0.2000								
20	$Q(\beta, \eta)$	0.0000	0.0000								
21	SP1	0.0000	0.0000								
22	SP2	0.0000	0.0000								
23	VM1	0.0000	0.0000	SP3							
24		0.0000	VM1								
25	SOLVER	0.0000	0.0000	0.00000	SOLVER: SET D25=0, CHANGING B26:C30						
26	A1	0.1481	0.0333	A2							
27	$\beta_1$	3.00000	4.0981	$\beta_2$							
28	$\eta_1$	-2.00000	-2.7321	$\eta_{2,1}$							
29	$V_1^*$	135.00000	126.8369	$V_2^*$							
30				-0.3660	$\eta_{2,2}$						
31	$K_1^*$	90.00000	90.0000	$K_1^*$							
32				10.0000	$K_2^*$						
33	VOLATILITY	0.2000	0.4472								
34	$\beta_1$	3.0000	1.3660	$\phi_2$							
35	ROV 1	18.2899	10.3129	ROV 2							
36	$\sigma_1^2$	$B6^2 + B7^2 - 2 * B9 * B6 * B7$									
37	$Q(\beta, \eta)$	$0.5 * (B19) * B27 * (B27 - 1) + B27 * (B13 - B14) - (B12 + B16 - B14)$									
38	SP1	$B27 * B26 * (B29 \wedge (B27 - 1)) * (B31 \wedge B28) - 1$									
39	SP2	$B28 * B26 * (B29 \wedge B27) * (B31 \wedge (B28 - 1)) + 1$									
40	VM1	$B26 * (B29 \wedge B27) * (B31 \wedge B28) - (B29 - B31)$									
41	ROV 1	$IF(B3 < B29, B26 * (B3 \wedge B27) * (B4 \wedge B28), B29 - B31)$									
42	$\sigma_2^2$	$(B27^2) * (C6^2) + ((1 - B27)^2) * (C7^2) + (C8^2) + 2 * B27 * (1 - B27) * C9 * C6 * C7 - 2 * B27 * C10 * C6 * C8 - 2 * (1 - B27) * C11 * C7 * C8$									

Figure 7.4 shows the results, using the backwardation principle so the  $J = 1$  stage is enumerated first, then the  $J = 2$  stage. The volatilities at each of the 2 stages,  $\sigma_1$ , and  $\sigma_2$  are evaluated, as are the parameters  $\phi_j$  for  $J = 1$ . The volatilities at each

stage increase in magnitude as the stage in question becomes more distant from completion. As expected, the parameter values  $\phi_j$  are all greater than one. Note that with these parameter values,  $\hat{V}$  increases with the distance of the stage from completion, and with the stage volatility, as does the excess of the  $\hat{V}$  over the assumed investment cost over each stage. The real option value (ROV), which is the option to continue the next stage if  $V < \hat{V}$ , and otherwise  $V$  less the remaining investment costs (or zero), decreases with the distance from the final state.

Figure 7.5 illustrates the matrix approach to solving the same problem as described in Adkins and Paxson (2013).

	A	B	C	D	E	F	G	H	I
1	<b>SEQUENTIAL MATRIX</b>	2 STAGES	T	STAGE	VOLATILITY	$\phi$	$V^\wedge$	$V^\wedge - \Sigma K_N$	ROV
2	Project value V	100	3.75	1	0.2000	3.0000	135.0000	45.0000	18.2899
3	$\theta V$	0	2.97	2	0.4472	1.3660	126.8368	26.8368	10.3129
4	$\sigma V$	20%	Input the correlations:						
5	Stage 1			V	K1	K2		Volatility	
6	$\theta K1$	0.04	V	100%	50%	50%		20%	
7	$\sigma K1$	20%	K1	50%	100%	0%		20%	
8	Failure probability: $\lambda$	0.0000	K2	50%	0%	100%		20%	
9	Stage 2			Assumes all V, K correlations are the same as in E10, Ks are not correlated.					
10	$\theta K2$	0.0400	$T_2$	$(1/(\$B\$14 - \$B\$3)) * \text{LN}(G3/\$B\$2)/2$					
11	$\sigma K2$	0.2000							
12	Failure probability: $\lambda$	0.0500							
13									
14	Risk-free rate	0.0400							
15	Threshold Levels								
16	$K1^\wedge$	90							
17	$K2^\wedge$	10							

The result is the same as in solving the two sets of equations. The expected investment timing at each stage is shown in C2 and C3, assuming a deterministic drift of V equal to the interest rate (and then for comparison with Geske, the result is divided by 2). This assumes some arbitrary process for the time that it takes V to reach  $\hat{V}$ , ignoring the fact that V is stochastic.

When the same Ts are used for the Geske compound European option over two stages, the ROV is 12, shown in Figure 1, (compared to 10.30 for A&P sequential American option over two stages). However, the comparison is between the Geske

model with only one source of uncertainty, and the A&P model with several sources of uncertainty including the possibility of total project failure in the current stage.

There are many other alternative combinations of differentials among stages of value volatility, investment cost volatility at each stage, and correlations at each stage that could be simulated, to illustrate the power and surprises of viewing sequential investment opportunities (and eventually investment requirements over stages) using this model as in Adkins and Paxson (2016).

## **SUMMARY**

Sequential investment options are appropriate when an investment program involves several stages, such as required initial expenditures (equivalent to a real option premium), a second phase of required investment expenditures (D), and a final development phase, when then the project values (V) are realized. The essential aspect of this characterized program is that managers have a choice about whether to pay the interim expenditure, and then the final development cost (K).

This chapter presents three real option valuation methods, starting with a simple European compound option, extended to a European compound exchange option, and then an American perpetual exchange option, allowing for several stages of investment expenditures (and critical values which justify making those expenditures).

## **EXERCISES**

### **EXERCISE 7.1**

Roger Action wants to achieve his lifetime goal of monetizing a brilliant real option model on sequential investments, but realizes that there are two critical stages left requiring large investment sums. The final stage requires software and marketing



costs in implementing a practical useful version of the model. The final stage is fairly simple with virtually no chance of failure, but both investment cost (=90) (increasing at 4% p.a.) and model value (=100) (increasing at 0%) are uncertain (volatility of 20%) but are not correlated. For the current stage, investment costs (=10) will increase at 4% p.a., are just as volatile and there is a 5% chance that the current stage will not succeed. The riskless interest rate is 4%, so  $\beta_1=3$ , and  $\phi_2=1.366$ . Roger assumes that  $\hat{K}_1=90$   $\hat{K}_2=10$ , so he needs advice on the level of  $\hat{V}_1$  and  $\hat{V}_2$ , and also the real option value at the current stage, since his wife wants him to sell this idea, and devote more time and effort to her.

The final stage model represents the investment opportunity for developing a project value  $V$  requiring the investment cost  $K_1$ . The real option value  $F_1$  of the investment opportunity, depending on the project value and the investment cost, is:

$$F_1 = A_1 V^{\beta_1} K_1^{\eta_1}, \quad (1)$$

where  $\beta_1$  and  $\eta_1 = (1 - \beta_1)$  are the power parameters for the two factors, and  $A_1$  denotes an unknown coefficient. The threshold level which justifies making the investment is:

$$\hat{V}_1 = \frac{\beta_1}{\beta_1 - 1} \hat{K}_1, \quad (2)$$

$$\text{with } A_1 = \beta_1^{-\beta_1} (\beta_1 - 1)^{\beta_1 - 1}. \quad (3)$$

At the current stage the real option value is:

$$F_2 = B_2 [F_1]^{\phi_2} K_2^{1 - \phi_2} \quad (4)$$

$$\text{Let } B_2 = (\phi_2 - 1)^{(\phi_2 - 1)} / \phi_2^{\phi_2}. \quad (5)$$

The value threshold which justifies commencing the stage 2 investment is:

$$\hat{V}_2 = \frac{\beta_1}{\beta_1 - 1} \left\{ \frac{\phi_2 (\beta_1 - 1)}{\phi_2 - 1} \right\}^{\frac{1}{\beta_1}} \hat{K}_1^{\frac{\beta_1 - 1}{\beta_1}} \hat{K}_2^{\frac{1}{\beta_1}} \quad (6)$$

## PROBLEMS

**PROBLEM 7.2** A bungalow in Putney has a restrictive covenant requiring the permission of the adjacent house owner in order to convert the bungalow into a modern house. That house owner is required to make extensive design and planning expenditures by the end of the next year prior to the construction of the new house. These expenditures and demolition costs are expected to be £150,000. A house of 3,000 square feet is envisioned, which currently would be worth £300 per square foot and costs £273 per square foot to build. The volatility of Putney houses is 20%, rental yield is 4% and interest rates are 4%. The redevelopment must occur at the end of five years. What is the value of this bungalow site? At what house value should the construction start?

**PROBLEM 7.3** A bungalow in Putney has a restrictive covenant requiring the permission of the adjacent house owner in order to convert the bungalow into a modern house. That house owner is required to make extensive design and planning expenditures by the end of the next year prior to the construction of the new house. These expenditures and demolition costs are expected to be £150,000, and along with construction costs are 50% correlated with housing prices. A house of 3,000 square feet is envisioned, which currently would be worth £300 per square foot, and costs £273 per square foot to build. The volatility of Putney houses is 20%, the same as the construction costs, the “yield” on renting such a house is 4%, construction cost escalate by 4%, and interest rates are 4%. The redevelopment must occur at the end of five years. What is the value of this bungalow site? At what house value should the construction start?

## **PROBLEM 7.4**

Willard Wang wants to enjoy the fruits of his research involving two expenditures (both equal to 50)  $K_1$  at the end of the first year and  $K_2$  at end of the second year. The current research price is 15, continuous cost is 10, the interest rate is 4% and the research yield is 4%. The research volatility is 20%. What's today's value of WW's

research, and at what research price should he make the first and second investment expenditures?

#### PROBLEM 7.5

Pixit & Dindyck are planning a superior real options product PROD that will indicate optimal timing for perpetual multi-stage projects. They estimate that the current value of PROD is 81, costs 90 to make in three stages (10 in the current stage, 30 in the middle stage) has a volatility of 20%, interest rates are only 5%, while the yield on the PROD is expected to be 2%. The failure rate of the current stage is 10%, 5% for the middle stage and there is no failure expected for the final stage. Advise P&D on this adventure.

#### PROBLEM 7.6

Pixit & Dindyck are planning a superior real options product PROD that will indicate optimal timing for perpetual multi-stage projects. This time they estimate that the current value of PROD is 87, costs 90 to make in three stages (10 in the current stage, 30 in the middle stage) has a volatility of 20%, cost volatility is 34%, with a -9% correlation of PROD value and cost. The yield on the PROD is expected to be 2%, with no yield for the investment cost. The failure rate of the current stage is 10%, 5% for the middle stage and there is no failure expected for the final stage. Advise P&D on this venture.

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## APPENDIX A Three-Stage Model

The extension of the sequential investment model to the  $J = 3$  stage is achieved by replication. The value of the option to invest at the  $J = 3$  stage  $F_3$  depends on the project value  $V$ , and the investment costs at the  $J = 1$ ,  $J = 2$  and  $J = 3$  stages,  $K_1$ ,  $K_2$  and  $K_3$ , respectively, so  $F_3 = F_3(V, K_1, K_2, K_3)$ . Using Ito's lemma, it can be shown that the risk neutral valuation relationship for  $F_3$  is:

$$F_3 = A_3 V^{\beta_3} K_1^{\eta_{31}} K_2^{\eta_{32}} K_3^{\eta_{33}}, \quad (7.32)$$

with a simplified characteristic root equation

$$Q_3 = \frac{1}{2} \sigma_3^2 \phi_3 (\phi_3 - 1) + \phi_3 (r + \lambda_2 - \theta_{K_3}) - (r + \lambda_3 - \theta_{K_3}) = 0. \quad (7.33)$$

$$\begin{aligned} \frac{1}{2} \sigma_3^2 &= \frac{1}{2} \sigma_V^2 \phi_2^2 \phi_1^2 + \frac{1}{2} \sigma_{K_1}^2 \phi_2^2 (1 - \phi_1)^2 + \frac{1}{2} \sigma_{K_2}^2 (1 - \phi_2)^2 + \frac{1}{2} \sigma_{K_3}^2 \\ &+ \rho_{VK_1} \sigma_V \sigma_{K_1} \phi_1 (1 - \phi_1) \phi_2^2 + \rho_{VK_2} \sigma_V \sigma_{K_2} \phi_1 \phi_2 (1 - \phi_2) \beta_3 \eta_{23} - \rho_{VK_3} \sigma_V \sigma_{K_3} \phi_1 \phi_2 \\ &+ \rho_{K_1 K_2} \sigma_{K_1} \sigma_{K_2} (1 - \phi_1) \phi_2 (1 - \phi_2) - \rho_{K_1 K_3} \sigma_{K_1} \sigma_{K_3} (1 - \phi_1) \phi_2 - \rho_{K_2 K_3} \sigma_{K_2} \sigma_{K_3} (1 - \phi_2). \end{aligned} \quad (7.34)$$

$$\hat{V}_3 = \left\{ \frac{\phi_3}{\phi_3 - 1} \frac{\phi_2^{\phi_2}}{(\phi_2 - 1)^{(\phi_2 - 1)}} \left[ \frac{\phi_1^{\phi_1}}{(\phi_1 - 1)^{\phi_1 - 1}} \right]^{\phi_2} \right\}^{1/\phi_1 \phi_2} \hat{K}_1^{(\phi_1 - 1)/\phi_1} \hat{K}_2^{(\phi_2 - 1)/\phi_1 \phi_2} \hat{K}_3^{1/\phi_1 \phi_2} \quad (7.35)$$

An alternative analytical solution to multi-stage sequential investments that does not require increasing probabilities of success is presented in Adkins and Paxson (2016), where there is a required differential among the stages of value volatilities, or drifts, or some other parameter values. The relative magnitude of  $\hat{V}_1$  and  $\hat{V}_2$  is determined from comparing (7.20) and (7.31):

$$\frac{\hat{V}_2}{\hat{V}_1} = \left\{ \frac{\phi_2(\phi_1 - 1) \hat{K}_2}{\phi_2 - 1 \hat{K}_1} \right\}^{\frac{1}{\phi_1}} \quad (\text{B1})$$

where  $\hat{K}_1 = \hat{K}_{11} = \hat{K}_{21}$  and  $\hat{K}_2 = \hat{K}_{22}$ . Since  $\phi_1 > 1$ , then for stage-2 investment to be justified earlier than stage-1 investment,  $\hat{V}_2 < \hat{V}_1$ , the following lower bound *LB* must hold:

$$\frac{\hat{K}_1}{\hat{K}_2} > \frac{\phi_2(\phi_1 - 1)}{\phi_2 - 1} > 1. \quad (\text{B2})$$

The  $Q_1$  function (7.15) is a quadratic expressed as:

$$\begin{aligned} Q_1(\beta_1, 1 - \beta_{11}) &= \frac{1}{2} \beta_1 (\beta_1 - 1) \sigma_1^2 + \beta_1 (\theta_{V_1} - \theta_{K_1}) - (r - \theta_{K_1}) \\ &= \frac{1}{2} \beta_1^2 \sigma_1^2 + \beta_1 (\theta_{V_1} - \theta_{K_1} - \frac{1}{2} \sigma_1^2) - (r - \theta_{K_1}) = 0, \end{aligned} \quad (\text{B3})$$

with the solution 
$$\frac{-b \pm \sqrt{b^2 - 4ac}}{2a} \quad (\text{B4})$$

where a, b and c are 
$$\frac{1}{2} \sigma_1^2, \quad (\theta_{V_1} - \theta_{K_1} - \frac{1}{2} \sigma_1^2), \quad -(r - \theta_{K_1}) \quad (\text{B5})$$

The  $Q_2$  function (7.29) is a quadratic expressed as:

$$Q_2 = \frac{1}{2} \sigma_{21}^2 \phi_2^2 + \phi_2 \{ \phi_1 \theta_{V_2} + (1 - \phi_1) \theta_{K_1} - \theta_{K_2} + \frac{1}{2} \phi_1 (\phi_1 - 1) \sigma_{21}^2 - \frac{1}{2} \sigma_{21}^2 \} - \{ r - \theta_{K_2} \} = 0 \quad (\text{B6})$$

with: 
$$\sigma_{21}^2 = \sigma_{V_2}^2 + \sigma_{K_1}^2 - 2\rho_{V_2 K_1} \sigma_{V_2} \sigma_{K_1} \quad (\text{B7})$$

The coefficients for this quadratic are:

$$\frac{1}{2} \sigma_{21}^2, \quad \phi_1 \theta_{V_2} + (1 - \phi_1) \theta_{K_1} - \theta_{K_2} + \frac{1}{2} \phi_1 (\phi_1 - 1) \sigma_{21}^2 - \frac{1}{2} \sigma_{21}^2, \quad -(r - \theta_{K_2}). \quad (\text{B8})$$

	A	B	C
1	<b>STAGE SPECIFIC RISKS and DRIFTS QUADRATIC SOLUTION</b>		
2	<b>INPUT</b>	<b>STAGE ONE</b>	
3	V	100.00	
4	K1	90.00	
5	$\sigma V1$	0.20	
6	$\sigma K1$	0.20	
7	$\rho V1K1$	0.50	
8	r	0.04	
9	$\theta V1$	0.00	
10	$\theta K1$	0.04	
11		<b>STAGE TWO</b>	
12	V	100.00	
13	K1	90.00	
14	K2	10.00	
15	$\sigma V1$	0.20	
16	$\sigma V2$	0.20	
17	$\sigma K1$	0.20	
18	$\sigma K2$	0.20	
19	$\rho V1K1$	0.50	
20	$\rho V2K1$	0.50	
21	$\rho V2K2$	0.50	
22	$\rho K1K2$	0.00	
23	r	0.04	
24	$\theta V1$	<b>0.0125</b>	
25	$\theta V2$	0.00	
26	$\theta K1$	0.04	
27	$\theta K2$	0.04	
28	<b>OUTPUT</b>		
29	$\sigma^2$	0.0400 B5^2+B6^2-2*B7*B5*B6	
30	b1	-0.0600 B9-B10-0.5*B29	
31	$\phi_1$	3.0000 (-B30+SQRT((B30^2)-4*0.5*B29*(-(B8-B10))))/(2*0.5*B29)	
32	A1	0.1481 (B31^(-B31))*((B31-1)^(B31-1))	
33	V1*	<b>135.0000</b> (B31/(B31-1))*B4	
34	K1*	90.0000 B4	
35	$\eta_1$	-2.0000 1-B31	
36	ROV1	<b>18.2899</b> IF(B3<B33,B32*(B3^B31)*(B4^B35),B33-B34)	
37	$\sigma^2$	0.2000 (B31^2)*(B16^2)+((1-B31)^2)*(B17^2)+(B18^2)+2*B31*(1-B31)*B20*B16*B17-2*B31*B21*B16*B18-2*(1-B31)*B22*B17	
38	b2	-0.1375 ((B23-B27)+B31*(B25-B24)+0.5*B31*(B31-1)*((B16^2-B15^2)-2*(B20*B16*B18-B19*B15*B17)))-0.5	
39	$\phi_2$	1.3750 (-B38+SQRT((B38^2)-4*0.5*B37*(-(B23-B27))))/(2*0.5*B37)	
40	A2	0.0323 (((B39-1)^(B39-1))/(B39^B39))*(((B31-1)^(B31-1))/(B31^B31))^B39	
41	V2*	<b>126.0918</b> (B31/(B31-1))*(((B39*(B31-1))/(B39-1))^(1/B31))*(B42^((B31-1)/B31))*((B43^(1/B31)))	
42	K1*	90.0000 B13	
43	K2*	10.0000 B14	
44	$\beta_2$	4.1250 B39*B31	
45	$\eta_1$	-2.7500 (1-B31)*B44/B31	
46	$\eta_2$	-0.3750 1-B44-B45	
47	ROV2	<b>10.2479</b> IF(B12<B41,B40*(B12^B44)*(B13^B45)*(B14^B46),B41-B43)	
48	LB	7.3333	
49	K1/K2	9.0000	

The parameter values are similar to the previous Figures except that there is no probability of failure over the stages, but the  $V_1$  drift in the second stage is 1.25% rather than 0.